

HIGHLY ACCURATE 3D FIELD GRADIENT COMPUTATION USING LOCAL POST-SOLVING

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Accurate computation of field quantities

To enhance the accuracy of finite element (FE) based computations of field and force quantities, a post-solving technique with superconvergent properties is used. These techniques use an analytical series expression for the magnetic field potential inside a closed region. The coefficients in the analytical expression for the magnetic field potential are evaluated using the FE solution as a boundary condition. Several applications have been investigated, both in 2D and 3D [1][2][3]. The derivative of the analytical expression can be calculated without numerical differentiation. This leads to a more accurate value for the flux density B . This digest presents the calculation of the derivatives of the flux density B , using the same principle, i.e. double differentiation of the analytical expression for the magnetic potential. This results in a highly accurate value for the field gradient (Oe/nm). This quantity is important in evaluating recording head performance, e.g. the edge write gradient in a notch write head [4].

Theory

Inside a closed spherical region without sources, the magnetic field potential $u(r,\theta,\phi)$ satisfies Laplace's equation. The general solution in spherical coordinates can be formulated as [3]:

$$u = \sum_{m=0}^{\infty} \sum_{n=0}^{\infty} [p_{mn} \cdot c_{mn}(\theta, \phi) + q_{mn} \cdot s_{mn}(\theta, \phi)] \cdot r^n \quad (1)$$

where c_{mn} and s_{mn} are the surface harmonic functions (determined by the associated Legendre polynomials of the first kind and the trigonometric functions). The coefficients p_{mn} and q_{mn} are determined using a FE solution as a boundary condition for (1) on a finite number of points on a sphere with radius R . Both the flux density B and its derivatives are related to the magnetic potential u and can be expressed in terms of the coefficients p_{mn} and q_{mn} :

$$(B_x, B_y, B_z) = -\mu_0 \cdot \left(\frac{\partial u}{\partial x}, \frac{\partial u}{\partial y}, \frac{\partial u}{\partial z} \right) = -\mu_0 \cdot (p_{11}, q_{11}, p_{01}) \quad (2)$$

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$$\left(\frac{\partial B_x}{\partial x}, \frac{\partial B_y}{\partial y}, \frac{\partial B_z}{\partial z} \right) = -\mu_0 \cdot \left(\frac{\partial^2 u}{\partial x^2}, \frac{\partial^2 u}{\partial y^2}, \frac{\partial^2 u}{\partial z^2} \right) = -\mu_0 \cdot (2p_{22} - p_{02}, 2p_{22} - q_{02}, 2p_{02}) \quad (3)$$

These and similar expressions for the other six cross-derivatives will be derived in the full paper.

Field of Application

As a typical application for this technique, Fig.1 shows the FE model of a notch write head where the field gradient $\partial B_y / \partial y$ is calculated along the airgap (y-axis is vertical). In Fig.2, the field gradient calculated using post-solving (solid curve) is compared to the one calculated using two numerical differentiations (dashed line curve). In the full paper, it will be shown that the post-solving technique assures an enhanced accuracy for the field gradient.

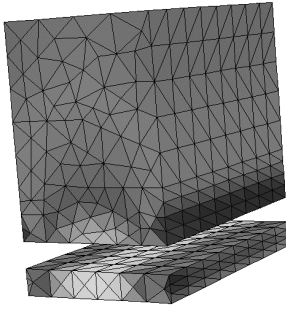


Fig.1 3D mesh of notch write head

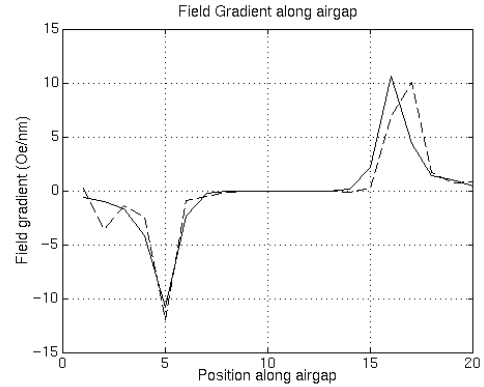


Fig.2 Field gradient along airgap.

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